



Loads Measurement and Validation of a 2.1-kW HAWT on a Fiberglass Composite Tower

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Motivation

Ongoing efforts to improve system dynamic modeling and prediction

Assess common industry practice loads derivation methods

Evaluate IEC 61400-2 Simplified Loads Approach

Address fatigue loads more comprehensively

Design Load Derivation Methods

1. Full-Scale Loads Measurements (Field)

- A 2.1-kW, free yaw, variable-speed, downwind machine
- An AnemErgonics, LLC 18-m multisection fiberglass composite tower
- Meteorological data recorded at hub height
- Tower strain measured at 0.8 m above tower hinge plate
- Full bending bridges in two orthogonal directions

2. Aeroelastic Modeling (FAST)

- FAST v 7.02 utilized
- Turbulent wind files, 3 seeds, with reference wind speeds of 2, 4...,24, 26 m/s
- Turbulence intensity of 18%
- Air density of 1.0 kg/m³ to match site conditions
- Tower drag not modeled

3. Simplified Loads Approach (SLA)

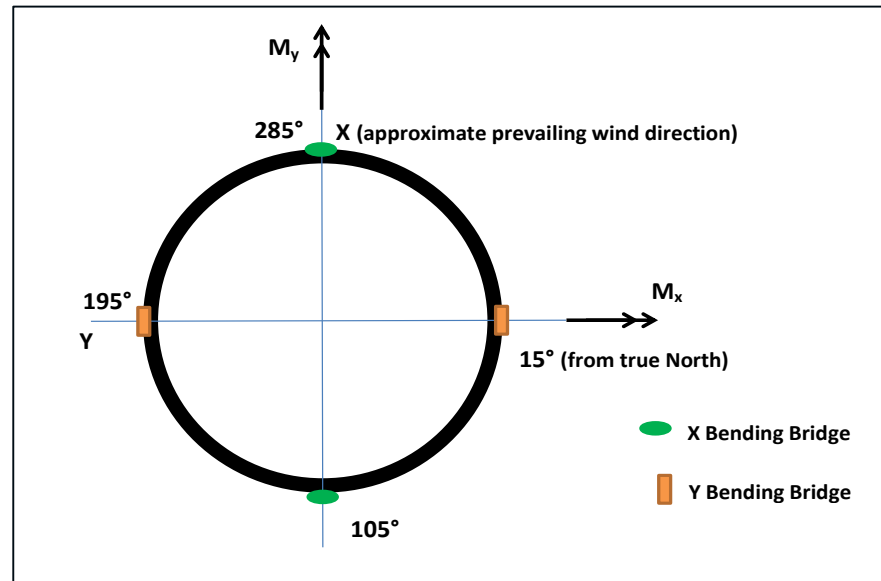
- IEC 61400-2 design load cases (DLCs) A (fatigue), H, and I (ultimate loads)
- Input parameters derived from the FAST model, preliminary test results, and turbine dimensions
- SLA load components used to determine the tower-base bending moment

Full-Scale Loads Measurements Approach



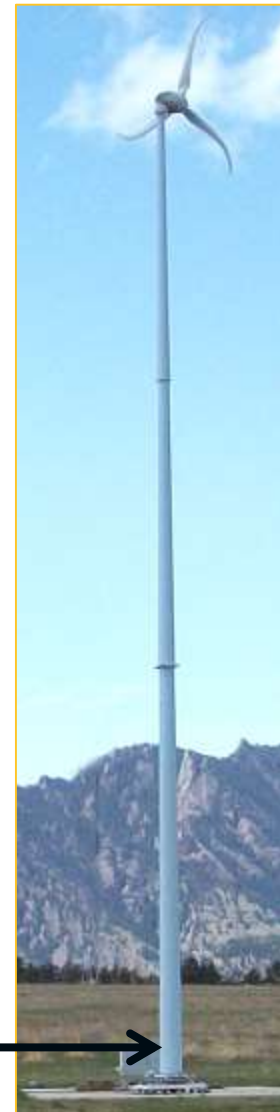
Met tower and instrumentation used for field test campaign (Photo by Scott Dana, NREL)

- Measurement sector of 223° to 333 ° of true north following IEC 61400-12-1
- Measurement methods and loads processing following IEC 61400-13
- Coordinate transformation applied to loads



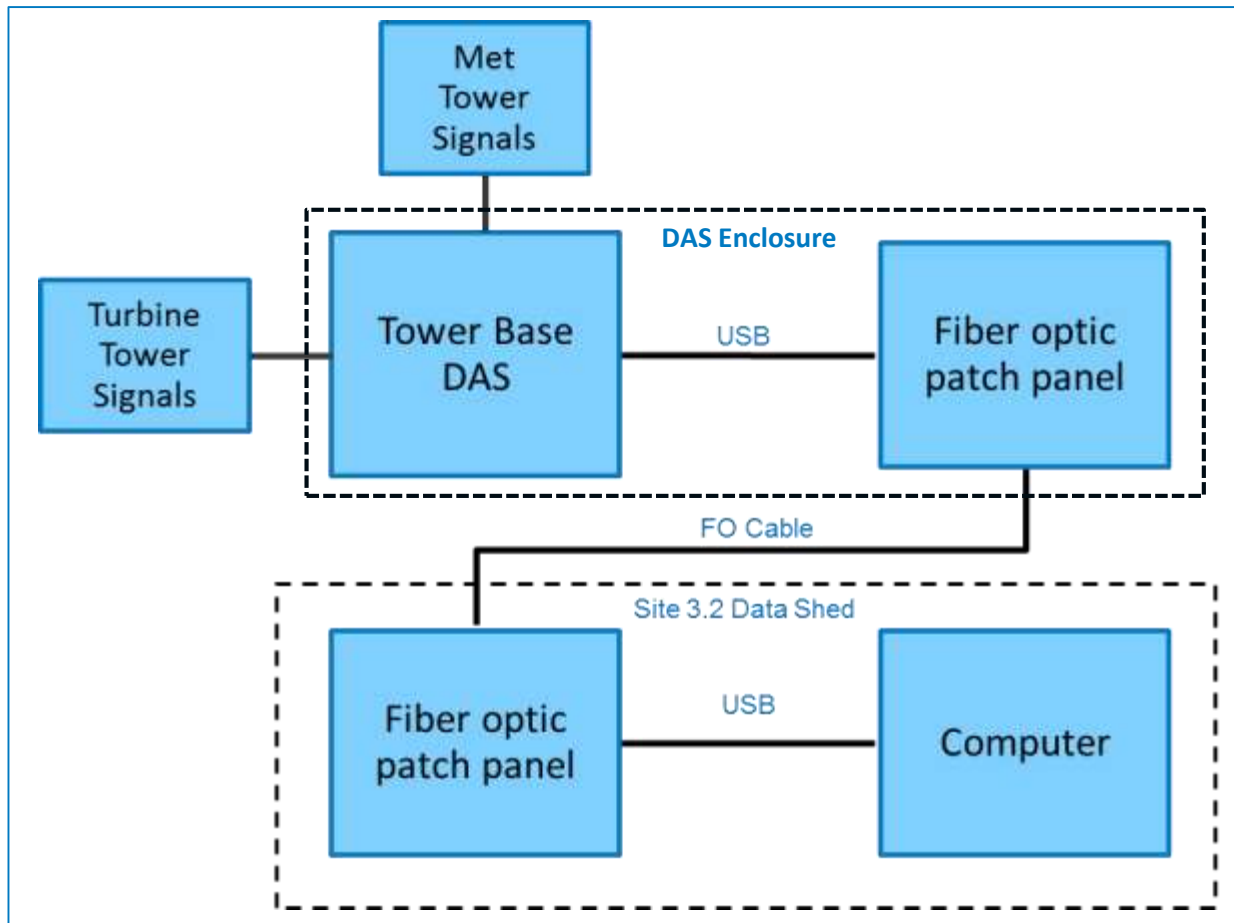
Tower Strain full bridge orientation and loads configuration

Tower-Base Bending Bridge Location



Test article used for full-scale loads measurement with identification of tower strain gage locations (Photo by Rick Damiani, NREL)

Measurement Data Acquisition System



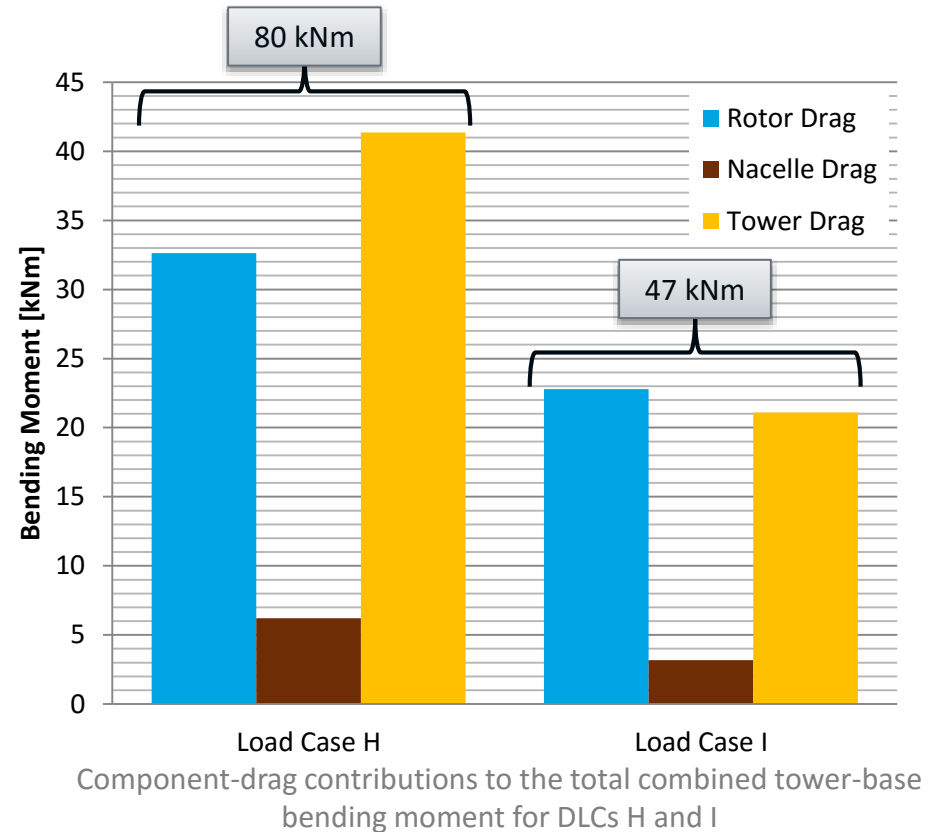
Communication one-line for tower loads DAS

- NI cDAQ Chassis and Input Modules
 - Sampled at 35 kHz
 - Stored at 100 Hz
- 1,332 10-Minute data files within measurement sector for Loads Calculations
- 3,482 10-Minute data files for Fatigue Calculations (all operating data)

Simplified Loads Approach – Maximum Bending Moments

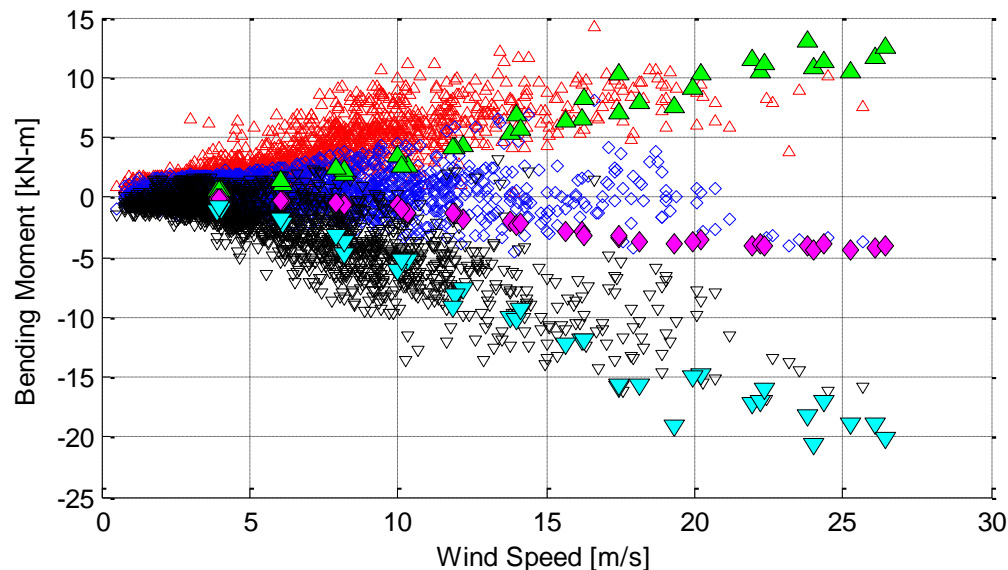
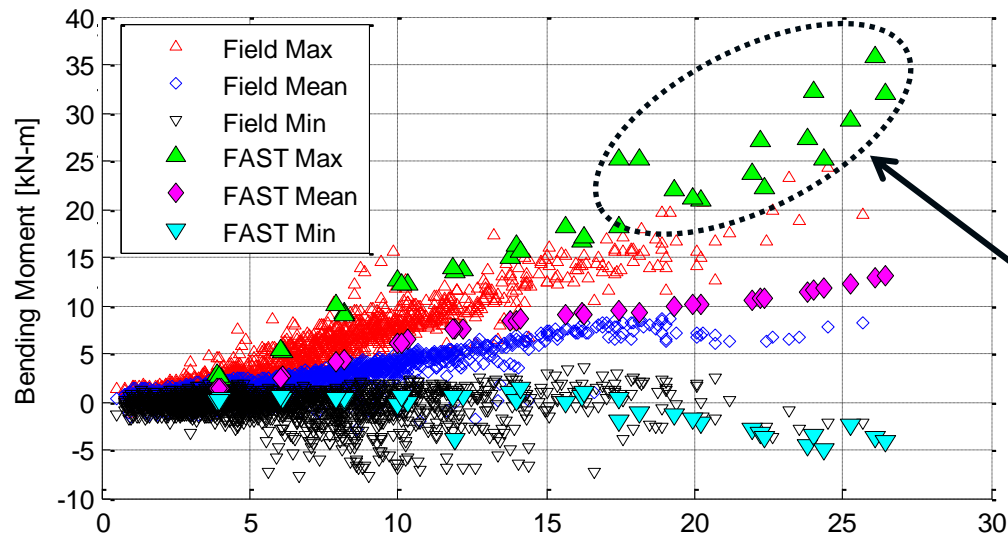
SLA DLCs for tower analysis:

- IEC 61400-2 DLC H
 - Extreme wind speed of 59.5 m/s
 - A normally parked turbine
 - Total Moment = 80 kNm
- IEC 61400-2 DLC I
 - 42.5 m/s wind speed
 - Maximum exposure (yaw mechanism failure)
 - A 'no-yaw-error' configuration in this case
 - Total Moment = 47 kNm



DLC H develops the greatest bending moment → Tower Design Driver

FAST and Field Bending Moments Results



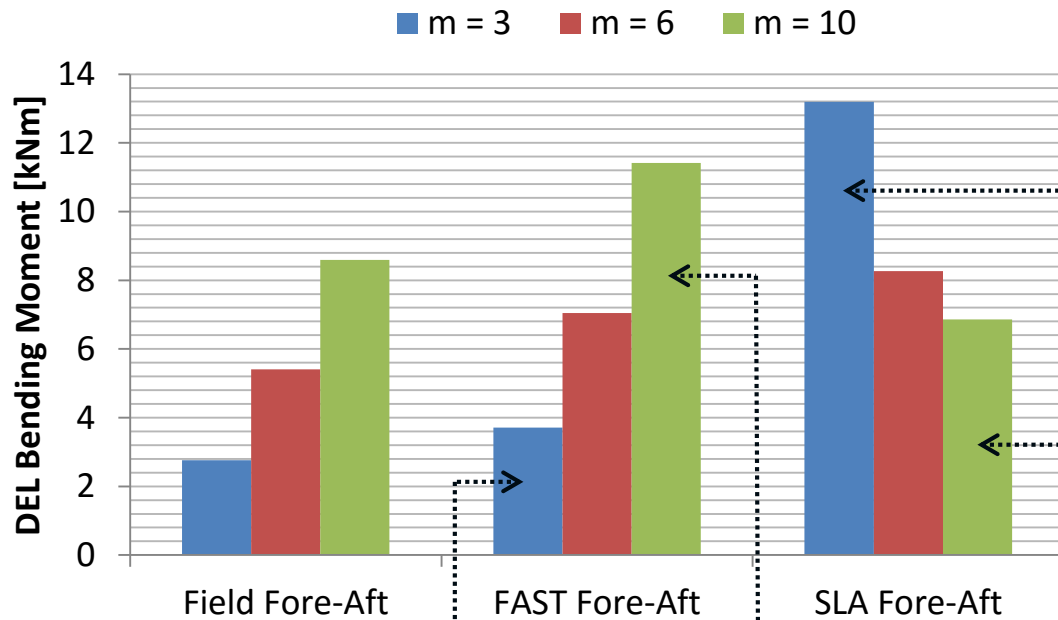
Ten-minute statistical comparison of the Field and FAST tower-base ultimate loads in the fore-aft (top) and side-to-side (bottom) directions

- Deviation between Field and FAST is likely a result of the actual turbine control system mitigating loads at high wind speeds (18 m/s and above)
- For the captured wind speeds FAST and field loads are within the load envelope of DLCs H and I
 - Less than 47 kNm (DLC I)

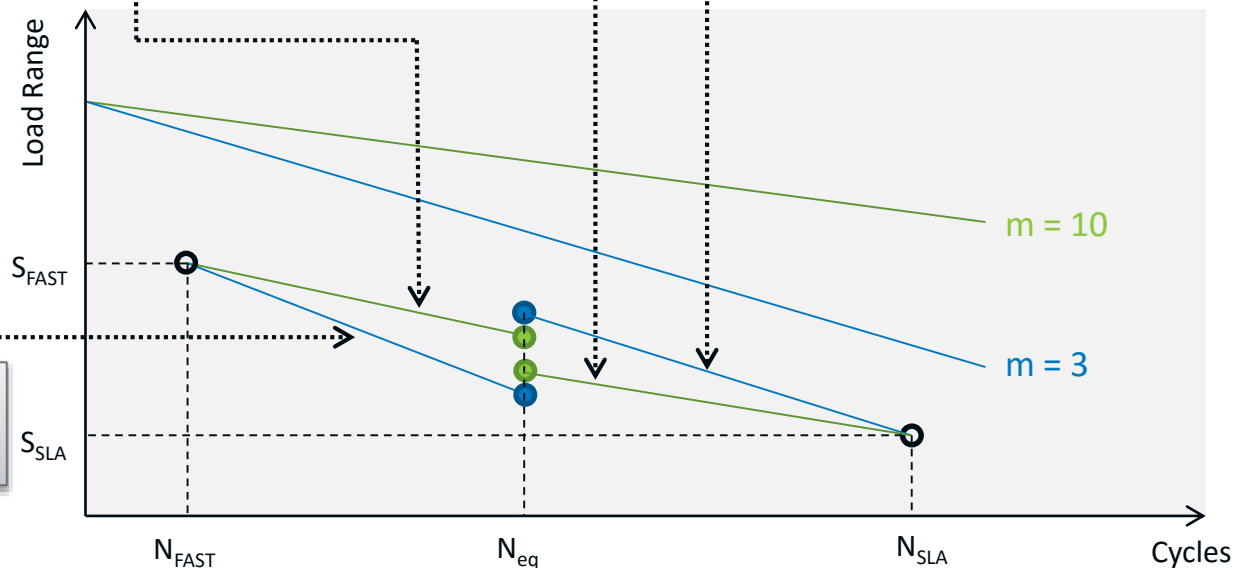


Loads extrapolation of the field-measured loads is required for a proper comparison with SLA results — a future work item of this study.

Fatigue Loads Comparison – Damage Equivalent Loads

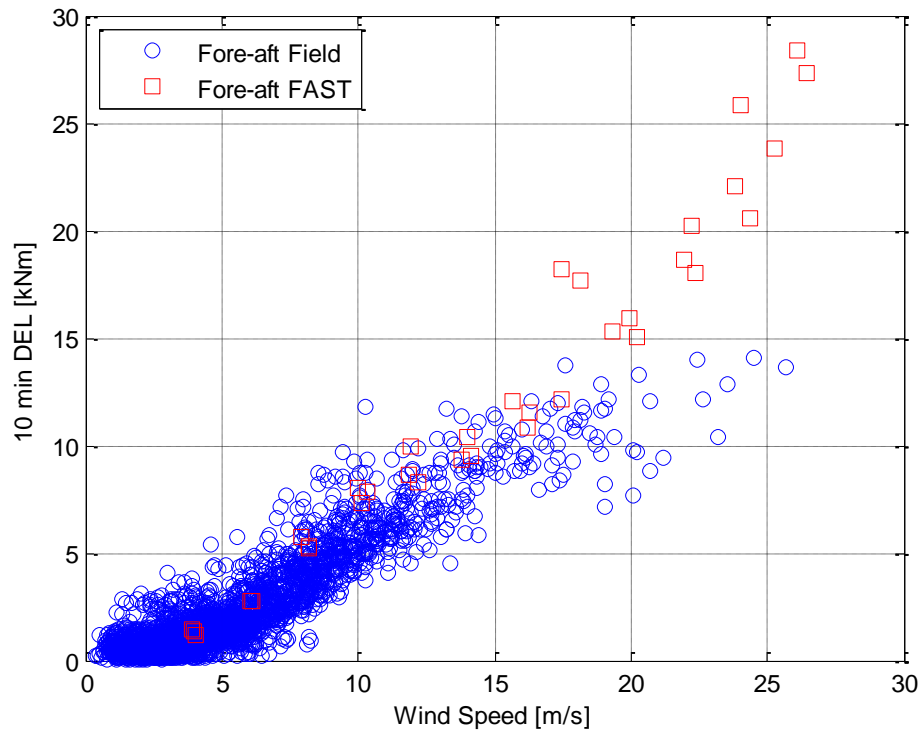


- Three different S-N curves
- Rayleigh distribution of wind speed
- 20-year design life
- SLA DELs by IEC 61400-2 DLC A
- Peak-to-peak thrust load
- 20-yr # of cycles @ rated rotor speed



Significant effect of material properties → S-N curve exponent!

Fatigue Loads Comparison Continued

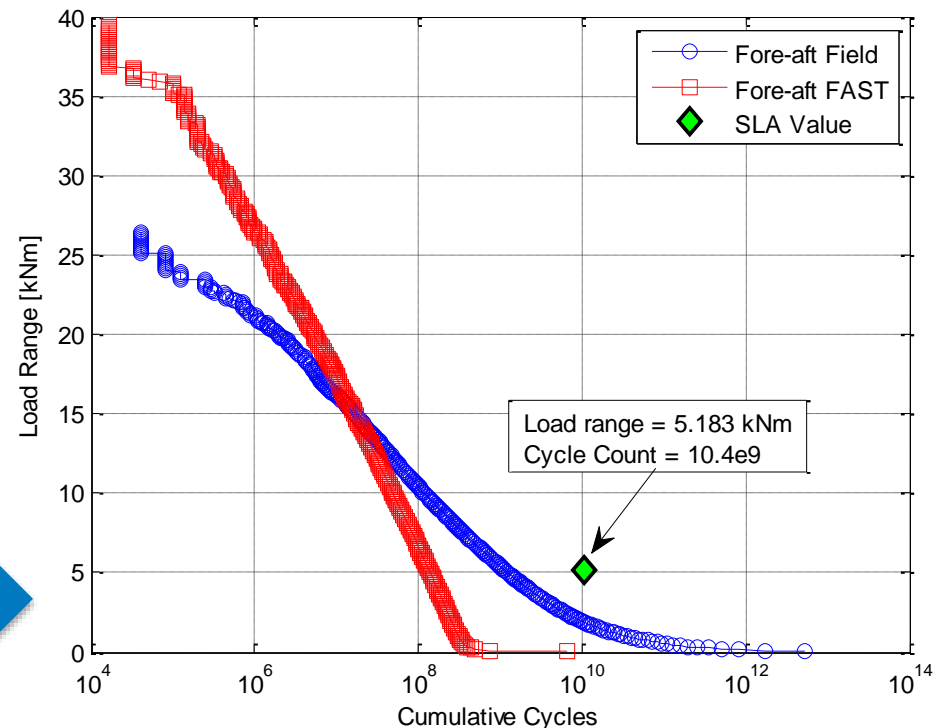


Short-term (10 minute) fore-aft tower-base bending moment DELs versus the mean wind speed for an S-N curve with $m = 10$

- The SLA DLC A yields a single fatigue load range value of 5.183 kNm, with a cycle count of $10.4e9$.



- Although similar, FAST's over-prediction of high-range loads compared to the field spectra are demonstrated.
- This outcome is consistent with the ultimate loads comparison.



Fore-aft tower-base bending moment cumulative fatigue spectra comparison of field-measured loads and FAST predictions

Final Remarks

This study focused on tower-base bending moments of a horizontal-axis wind turbine to provide an indication of the overall performance of the load derivation methods. Notable outcomes include the following:

- The SLA DELs are different than those calculated from the Field and FAST data;
 - High dependence on the assumed S-N curve slope and the number of cycles.
 - SLA DEL more conservative for steel ($m = 3$ to 6) and less conservative for composites ($m = 10$).
- Better agreement between the field and FAST predictions for side-to-side than for fore-aft bending at high wind speeds;
 - Likely caused by a lower fidelity turbine control model used in the FAST simulations.
- The fatigue spectra reveals FAST's over-prediction of large cycles.
- SLA does not comprehensively address fatigue;
 - Conservative and coarse → one load range at one cycle count.
- We recommend that this study be repeated with wind turbines of different configurations and sizes, and that field load extrapolation be conducted.

Acknowledgements

- The Authors of this work would like to sincerely thank Paul Migliore of AnemErgonics for allowing his tower and turbine to be used for the field measurement campaign of this study.
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Thank you!

Questions?

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